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(54) Title: GLASS ARTICLE			
(57) Abstract			
<p>A glass coating composition including an effective amount of at least one inorganic or organic polymeric component; and at least one reinforcing component incorporated therein; the glass coating composition being such that when coated on a glass substrate it strengthens and toughens the article.</p>			

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GLASS ARTICLE

The present invention relates to glass articles including toughened glass articles and to a method of preparing such glass articles.

Silica based glasses, including the widely-used soda-lime container glass, are isotropic elastic solids. They are chemically homogeneous, with all the constituent atoms strongly bonded to one another, but with no long-range or periodic order.

Estimates based on the nature of the interatomic forces indicate that strains of up to 20% should occur before rupture occurs: this is equivalent to strengths in the range 10-20 GPa. For normal samples, observed strengths usually are less than one hundredth of this theoretical level; moreover, samples which have received nominally identical treatment show a wide variation in their individual strengths.

It is well established that fracture of glass occurs at pre-existing flaws or microcracks, and this limits the attainable strength. Most glass articles possess surface microcracks which have been produced by abrasion, indentation or impact of the surface by another hard body, or by another glass article. The mechanism of microcrack initiation in pristine surfaces has yet to be established, however. Even when mechanical damage to a glass surface has been avoided, the strength may not be any larger: in this case, the flaws responsible may be foreign particles which have become fused to the surface and which generate microcracks around themselves as a result of differential thermal expansion when the body is cooled. Such surface inclusions may be airborne

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dust particles present during the heat treatment of the glass, and temperatures well below the softening point of the glass will suffice to develop strongly-bonded inclusions, which then act as significant strength-limiting flaws. Also, 5 atmospheric moisture acts detrimentally on a glass surface, producing corrosion products; these are a form of foreign inclusion, and have the same strength-limiting effect.

Some attempts in the prior art to increase the strength of glass have been partially successful. These 10 procedures are based on the fact that if the glass surface is placed under compression, extra work must be done to overcome this compression before any pre-existing microcrack can be widened and thereby produce catastrophic failure. One such prior art procedure compresses the surface of a glass body by 15 chilling with an air blast at a time when the glass was plastic. Then, under normal cooling, the thermal shrinkage of the bulk compresses the hardened surface layer. This procedure has been much used for toughened glass plates.

In another procedure, the sodium in the surface 20 layer of glass is exchanged for potassium in a molten salt bath. Since the potassium ions occupy a greater volume than the sodium ions they have replaced, the surface layer is placed under a compressive stress. This procedure is costly, however, and cannot be applied reasonably to glass containers 25 that are made in large numbers.

Accordingly, it is an object of the present invention to overcome, or at least alleviate, one or more of the difficulties related to the prior art.

Accordingly, in a first aspect there is provided a glass coating composition including an effective amount of at least one inorganic or organic polymeric component; and

5 at least one reinforcing component incorporated therein.

The glass coating composition according to the present invention, when coated on a glass article, strengthens and toughens the article. The coating 10 advantageously adheres strongly to the glass substrate and possesses a high tensile strength of itself.

Whilst we do not wish to be restricted by theory, it is postulated that the coating formed from the glass coating composition lies across any pre-existing, strength-limiting 15 flaws in the glass surface. Under the action of any applied tensile load, the stress across any flaw would then be carried by the coating. Thus, extra work would have to be done before the load carrying effect of the coating broke down, which would then allow the microcracks in the glass to 20 widen and cause failure of the glass.

Additionally, the coating formed from the glass coating composition may protect the glass surface from abrasion, indentation, or any other such damage leading to the production of strength limiting flaws.

25 The at least one inorganic or organic polymeric component of the glass coating composition may be of any suitable type which will provide the required high tensile strength. A water soluble or water insoluble polymer may be used. Where a water solubl polymer is used the coating

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composition may be rendered water resistant as discussed below. A natural or synthetic organic polymer may be used as the polymeric component. A synthetic organic polymer may be selected from acrylic polymers including acrylate and methacrylate polymers or copolymers, acrylamide or methacrylamide polymers or copolymers thereof, urethane polymers or copolymers thereof, alkyd resins, or mixtures thereof.

Preferred acrylic polymers include polyacrylamide and polymethylmethacrylate.

Alkyd resins ("Glyptal" resins), may be used alone, or with the inclusion of one or more copolymers to modify their properties in a manner known per se. These resins may be provided in a form that is soluble in common organic solvents such as alcohol, applied to the glass, dried, then converted to the final crosslinked or cured form thermally at temperatures near 200°C ("stoving varnishes"), or crosslinked with reagents such as melamine to further modify the properties according to known art. Alkyd resins are obtainable commercially in an extremely wide range of formulations, and admixtures with copolymers and crosslinking agents.

The preferred polyurethanes may be selected from the large range of formulations available commercially.

Polyurethane is known to have excellent adhesion to glass, and has been proposed as a useful coating (e.g. Vapocure process). There is a wide range of polyurethane products available and a correspondingly wide range of properties. For the present application, a commercial

two-part coating material was purchased (Epiglass reaction lacquer). Preliminary trials showed that this coating formed hard adherent films on freshly fired slides.

Polyurethanes are produced from a reaction between a polyhydroxyl compound (polyol) and a polyfunctional isocyanate. Typical reactants could be propylene glycol and toluene diisocyanate with a catalyst of tin octoate. The commercial two-part PU coatings contain partly polymerised polyol/diisocyanate: one part has unreacted hydroxyl groups and catalyst, the other part has an excess of isocyanate. When the two components are mixed they react to form a gelatinous solid in about an hour; reaction then continues to form a rigid polymer. Complete reaction at room temperature takes about 3 days.

The period of 3 days required to achieve complete reaction was inconvenient, so further investigations have been conducted at various temperatures and times to investigate thermal acceleration of the polymerization. It was found that heating to 80°C for 2 hours was sufficient to give a tough adherent film.

A protein polymer for example a casein polymer may be used as a natural polymeric component.

Alternatively, or in addition, a low melting silicon polymer may be used. A low melting glass may be used.

The at least one polymeric component may be present in any suitable effective amounts. The polymeric component may comprise from approximately 40 to 95% by weight, based on the total weight of the glass coating composition. A polymeric component content of about 50 to 95% by weight is

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preferred.

The at least one reinforcing component of the glass coating composition may have a platelet-type structure. The reinforcing component having platelet-type structure may be a silicon carbide or vermiculite product, for example an exfoliated vermiculite.

The reinforcing component may alternatively or in addition include a component having a fibrous structure, organic, inorganic or mineral fibres, preferably high-modulus whiskers or fibres. The reinforcing component having a fibrous structure may include silicon carbides, silicon nitrides, alumina, metals or mixtures thereof.

However, it is preferred that silicon carbide (SiC) including silicon carbide whiskers are not used in conjunction with polyacrylate polymers, alkyd resins.

A vermiculite product has the advantage that the particles are platelets typically approximately 5 m diameter and about 3nm thick, which do not represent any biological hazard, as may be encountered with product having a fibrous structure. Preferably, flakes would all lie parallel in a coating and be bonded to each other, and to the glass surface by the polymeric component. Where whiskers or fibres are present, these may be in any suitable configuration including felts, oriented weaves and lay-ups so as to provide desired mechanical properties to the coating.

The reinforcing component may be present in the glass coating composition in any suitable effective amount. The reinforcing component may be present in amounts of from approximately 5 to 60% by weight, based on the total weight

of the glass coating composition. A reinforcing component of approximately 5 to 40% by weight based on the total weight of the glass coating composition is preferred.

In a preferred aspect of the present invention the glass coating composition may further include an effective amount of at least one coupling agent.

The at least one coupling agent may function to improve adhesion of the polymeric component to the reinforcing component and/or to the glass substrate when, in use, the coating composition is coated onto such a substrate. The coupling agent may also function to improve the water resistance of the coating on curing.

The at least one coupling agent may be a silane product. An amino silane product may be used. (N,N-diethyl-3-aminopropyl)trimethoxysilane is preferred.

The at least one coupling agent may be present in the glass coating composition in any suitable effective amount. The at least one silane coupling agent may be present in an amount of from approximately 0.1 to 1% by weight based on the total weight of the glass coating composition.

In a further preferred aspect of the present invention, where a water soluble polymeric component is used, the glass coating composition may further include an effective amount of at least one cross-linking agent. The cross-linking agent may be a heat-, or radiation-curable cross-linking agent. A cross-linking agent such as a glyoxal formaldehyde may be used. The at least one cross-linking agent may be present in the glass coating composition in any

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suitable effective amount. The cross-linking agent may be present in amount of from 0 to approximatley 50%, preferably approximately 5 to 50%, more preferably approximately 7.5% to 10% by weight based on the total weight of the glass coating composition.

5

The glass coating composition according to the present invention may further include other compounding ingredients. Compounding ingredients such as colourants, fillers, solvents, dispersants, surfactants, extenders, and the like may be included.

10

The glass coating composition may be provided in the form of a solution or dispersion in a suitable solvent. An aqueous solvent or organic solvent or mixtures thereof may be used. An alcohol solvent, e.g. methanol or ethanol may be used. An aqueous solution is preferred.

15

In a preferred form the glass coating composition includes approximately 40 to 70% by weight of polyacrylamide; approximately 30 to 60% by weight of vermiculite; and approximately 0.1% to approximately 0.5% by weight of (N,N-diethyl-3-aminopropyl)trimethoxysilane.

20

In a further preferred form the glass coating composition may include

approximately 80 to 95% by weight of a polyurethane polymer; and

25

approximately 5 to 15% by weight silicon carbide.

In a further aspect of the present invention there is provided a toughened article including a glass article, and a glass coating on at least one surface thereof,

formed from a glass coating composition including
an effective amount of at least one inorganic or
organic polymeric component; and
at least one reinforcing agent incorporated therein;
the glass coating being such that when coated on the
glass article, it strengthens and toughens the article.

The glass article may be formed from a silica based
glass. The glass article may be formed from a soda-lime type
glass. The glass article may be a shaped article. The glass
article may be a container such as a bottle, jar or like
vessel.

The glass article may be subjected to a surface
purification step prior to application of the coating. The
glass article may be prepared for coating by way of a
cleaning or other step as discussed below.

The glass coating composition may include
approximately 40 to 70% by weight of polyacrylamide;
approximately 30 to 60% of vermiculite; and
approximately 0.1% to approximately 0.5% by weight
of a coupling agent, preferably (N,N-diethyl-3-aminopropyl)-
trimethoxysilane.

Alternatively, the glass coating composition may
include

approximately 80 to 95% by weight of a polyurethane
polymer; and
approximately 5 to 15% silicon carbide.

In a still further aspect of the present invention
there is provided a process for preparing a toughened article
including

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providing a glass article; and
a glass coating composition including
an effective amount of at least one inorganic or
organic polymeric component; and
5 at least one reinforcing component incorporated
therein;

the glass coating composition being such that when
coated on a glass substrate it strengthens and
toughens the article;

10 contacting the surface of the glass article with the
glass coating composition; and
drying the coated glass article so formed.

The glass article may be a glass container,
preferably a soda-lime type glass container as discussed
15 above.

The glass coating composition may be provided in the
form of an aqueous solution.

In a preferred form the glass coating composition
may further include at least one coupling agent. Where a
20 coupling agent is present, the process for preparing a
toughened article may include the preliminary step of
mixing the coupling agent with the polymeric
component and at least one reinforcing component for
a time sufficient to allow the coupling agent to
hydrolyse and/or to interact with the reinforcing
25 component prior to contact with the surface of the
glass article.

In a further preferred form, the at least one
reinforcing agent of the glass coating composition includes

exfoliated vermiculite. Where an exfoliated vermiculite is present, the process for preparing a toughened article may further include the preliminary step of

5 subjecting the vermiculite to a conversion process to produce an exfoliated vermiculite.

For example, the vermiculite may first be reacted with sodium chloride to form a sodium vermiculite. The sodium vermiculite may then be reacted with an N-butylamine hydrochloride to form the final exfoliated product.

10 In a still further preferred form, the process for preparing the toughened article may include the preliminary step of

subjecting the glass article to a surface preparation step.

15 The surface preparation step may include a physical or chemical cleaning step. Various solvents, acidic or basic polishers or etchers may be used. Alternatively or in addition an electrical discharge treatment may be included.

20 However, the most effective surface preparation step includes a heat treatment step. Preferably, the glass article is subjected to a firing in air at elevated temperature for a time sufficient to clean the surface. The heated glass may be then subjected to slow cooling, for example at room temperature.

25 The heat treatment step may be conducted at temperatures of approximately 350 to 450°C and above. Preferably a temperature of 400°C is preferred. Lower firing temperatures were found to be ineffective. Similarly, temperatures significantly higher than 450°C are to be

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avoided as there is a risk of compositional changes in the surface.

These surface preparations may be combined with various storage procedures to minimise atmospheric corrosion prior to coating of the freshly cleaned surfaces. For example, the glass articles may be stored under dry nitrogen after cleaning.

As stated above, the glass coating composition may preferably be provided in the form of an aqueous solution. The aqueous solution of the glass coating composition may be coated onto the surface of the glass article in any suitable manner. The glass coating composition may be coated onto the surface as a film for example using kiss coating, doctor rolls, gravure rolls, immersion coating techniques or similar techniques. The glass coating composition may be sprayed onto the glass surface in any known manner.

Once the glass coating composition is coated onto the surface, the film so formed may then be dried to remove excess solvent. Drying times and temperatures will vary depending, for example, on the composition of the composition and thickness of coating. The drying step may be conducted in air at room temperature for a period of approximately 12 to 48 hours, preferably for approximately 24 hours.

In a preferred aspect of the present invention, the process of preparing the toughened article may further include the further step of curing the coated glass article. The curing step may take any suitable form depending on the cross-linking agent present. Where the natural or synthetic organic polymer is a curable polymer, the curing step may

include heating the coated glass article at elevated temperature for a period sufficient to provide substantially complete cure. Temperatures of the order of 75 to 100°C, preferably approximately 80 to 90°C may be used.

The present invention will now be more fully described with reference to the accompanying examples. It should be understood, however, that the description following is illustrative only and should not be taken in any way as a restriction on the generality of the foregoing description.

EXAMPLE 1

(a) Test Rig

Glass microscope slides obtained commercially were used for testing. Strength testing of these, or of coated glass slides by standard 4-point bend procedures would be futile since the slides have cut edges and thus extensive arrays of strength-limiting flaws around these edges produced by the cutting process. These would control the apparent strength of any slide, and the results would be atypical of the glass itself. Flame polishing of the edges could reduce this effect, but this procedure would lead to evaporative loss of sodium from the glass, and the consequent compositional change would again lead to spurious results.

The strength testing rig used consisted of two rings of different diameters that pressed on each side of the glass surface. The rings were constrained to be coaxial by a suitable jig, which was placed in a standard testing machine (Instron). This test rig was thus a biaxial 4-point bend machine.

Fracture of the test slides was confined to the

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region inside the larger ring, so that the effects of the edges were eliminated or minimised. In each case, the test slide was coated on the compressive side with transparent adhesive tape so that the pieces could be retained and the 5 origin of fracture confirmed to be within the test ring.

Test slides were indented with a Vickers diamond indenter at 1 Kg load so as to make a single flaw that would control the strength of the slide. In all test cases, it was confirmed that the fracture originated at this flaw. The 10 purpose of this procedure was to ensure a reasonably constant base value for the strength of untreated glass, so that the effect of any coating would be immediately apparent. Also, any increase in strength above the base value resulting from any applied coating would represent a toughening effect due 15 to that coating.

(b) Preparation of exfoliated vermiculite

In accordance with a known procedure, natural vermiculite is converted to the sodium form by refluxing 400g in 1000 ml water containing 390g sodium chloride for 24 20 hours. The product is washed with water to remove chloride.

The sodium vermiculite is converted to the n-butylamine form by reaction with n-butylamine hydrochloride. The sodium vermiculite is refluxed for 24 hours in a solution consisting of 1000 ml water, 400ml 25 n-butylamine and sufficient (about 400ml) concentrated hydrochloric acid to make the pH 5.2

The n-butylamine product is repeatedly washed until it swells to several times its original volume. It is then milled in a high-speed blender or stirrer producing high

shear. The final product is a nacreous sol of platelets approximately 5 μm diameter and 2nm thick. This is concentrated by centrifugation to about 20% solids by weight.

5 (c) Cleaning of test glass slides

The most effective procedure was found to be a firing in air to 400°C for one hour followed by a slow cooling to room temperature immediately before coating. Lower firing temperatures were ineffective, whilst at higher temperatures there was the risk of compositional changes in 10 the surface because of component volatility (resulting in spurious mechanical properties) or healing of the artificial indentation flaw.

In a preferred form of the invention, a coating consisting of 60% by weight of polyacrylamide (PAA), and 40% 15 by weight of a reinforcing filler of exfoliated vermiculite flakes is applied to freshly cleaned container glass.

Thus 14.3g of an aqueous solution containing 20.75% by weight of P-26 PAA (Cyanamid Corp.) is mixed with 10.7g of 20 18.47% vermiculite sol and 50g of water. After thorough mixing, 0.05g of (N,N-diethyl-3-aminopropyl)trimethoxysilane (DEAPTMS) is added as a coupling agent. The DEAPTMS is allowed to hydrolyse and interact with the vermiculite for 24 hours before the mixture is applied to the glass.

The mixture is applied to freshly cleaned glass as a 25 film approximately 0.1mm thick by means of a Doctor Blade apparatus. The film is allowed to dry in air at room temperature for 24 hours, then cured at 85°C to render the coating water resistant.

The modulus of rupture (MOR) measured for indented

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uncoated glass slides was 56 ± 2 MPa: the MOR measured for indented slides coated as above was 87 ± 4 MPa, a significant enhancement.

MOR measurements for slides coated with
5 PAA/vermiculite compositions varying from 0 to 100% PAA showed that there was a broad maximum in the strength enhancement, and that the composition with 60% PAA was close to optimum.

EXAMPLE 2

10 Pu/SiC composites were prepared by adding SiC whiskers to freshly mixed PU resin. It was intended to apply composites of 3 different whisker amounts as well as unfilled PU to standard cleaned slides and acid washed slides. SiC whiskers were dispersed ultrasonically in the resin, since
15 simple mixing was ineffective.

The quantity of SiC whiskers that could be added to the PU resin was limited to a narrow range by the viscosity requirements of the film spreader. The unreinforced PU coating was applied by brush.

20 The complete coating procedure used was as follows:

- (a) A set of slides were fired at 400°C and cooled.
- (b) The slides were Vickers indented at 1 Kg.
- (c) The slides were refired at 200°C and cooled.
- (d) Immediately after the last firing the slides were mounted for coating.
- (e) A small quantity of the PU resin was mixed and the whiskers were added.
- (f) The slides were coated on the film spreader.
- (g) After 2 hours at room temperature the samples were

heated to 80°C for 2 hours.

(h) The coated samples were tested in the normal way on the biaxial rig.

A glass coating consisting of 94% to 91% by weight of polyurethane, and 6% to 9% by weight of reinforcing filler of silicon carbide whiskers is applied to freshly cleaned container glass.

Thus 8.8g of silicon carbide whiskers (Tateho Corp., Japan: 0.5 μm diameter, aspect ratio 10) were added to 91.2g of freshly-mixed two-part liquid polyurethane material (Epiglass Reaction Lacquer) and dispersed uniformly in an ultrasonic bath. Test glass was cleaned by firing at 400°C, provided with a strength-limiting flaw by indenting at 1Kg, refiring at 200°C, and coated with the mixture to a thickness of approximately 0.1mm. The test glass specimens were kept at room temperature for 2 hours to allow the coating mixture to set, then heated at 80°C for 2 hours to effect a full thermal curing of the polyurethane.

Additionally, test glass was prepared and coated as above, but using no whiskers in the polyurethane.

Also, test glass was prepared as above, but provided with no coating.

The MOR measured for indented uncoated glass was 56 \pm 2 MPa: the MOR measured for glass coated with polyurethane alone was 70 \pm 4 MPa: the MOR measured for glass coated with polyurethane containing 8.8% by weight silicon carbide whiskers was 115 \pm 19 MPa, a significant enhancement.

The area under the stress vs., displacement curves produced for each specimen in the fracture testing rig is a

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measure of the work of fracture, or toughness of the test specimen. Typical stress vs. displacement curves for uncoated indented glass, indented glass coated with polyurethane only and indented glass coated with polyurethane containing 8.8% by weight silicon carbide whiskers are shown in Figures 1, 2 and 3. The relative areas under the curves are in the ratio 1.0 : 2.1 : 40.0 respectively, so that compared to uncoated glass, the coating of polyurethane alone toughens the glass by a factor of 2.1, while the silicon carbide whisker/polyurethane coating toughens the glass by a factor of 40, a substantial increase.

Further, the decay of the stress/displacement curve to zero at a displacement near 1.2mm, for glass coated with silicon carbide whiskers/polyurethane, of which Figure 3 is a typical example, does not represent failure of the test piece, as does the corresponding parts of the curves in Figures 1 and 2. Here instead, the stress applied by the testing machine was removed because the test piece had deformed (without failure) to such an extent that the testing rig no longer performed its function properly, a further demonstration of the resistance to failure supplied by this coating. On relief of the stress, the test piece returned to its original form. For calculation of the MOR, the largest value of the applied stress observed was used, since no stress at rupture per se could be determined.

All specimens were examined microscopically after testing. Uncoated glass and glass coated with polyurethane alone had fractured cleanly and in the manner typical of a brittle material. There was some crack branching in the

coating layer, an energy absorption process that accounted for the small increase in toughness of glass so coated. Microscopical examination of the glass coated with silicon carbide whiskers/polyurethane after fracture testing showed
5 that the glass itself had a high density of fine cracks originating from the indentation: the production of these would have required far more work than that required to produce a single crack. The integrity of the piece was maintained by the coating. Also, cracks in the coating were
10 heavily branched, indicative of strong energy absorption or stress dissipation processes occasioned by the presence of the whiskers, while there was evidence that additionally, resistance to the widening of cracks in the coating under stress was provided by the whiskers bridging across such
15 cracks, so that energy was absorbed by whisker pull-out, a well-known toughening process.

Similar measurements made on glass similarly prepared and coated with polyurethane containing 6.2% by weight of silicon carbide whiskers gave results that did not differ significantly from those described above for
20 polyurethane containing 8.8% by weight of silicon carbide whiskers.

The test results for the PU/SiC composites are shown in Tables 1 to 7 and illustrated in Figures 4 to 10,
25 respectively.

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TABLE 1

As Fired Slides, Uncoated

Indented/Refired these slides were fired at 400°C

then indented then reheated to 200°C.

5 No coating was applied.

	SAMPLE		SAMPLES		
	NUMBER	DEPTH	LOAD	MOR (MPA)	21
19	1	0.94	98	54	WEIBULL
	2	0.94	103	57	MEAN: 30.28
	3	0.92	104	60	
	4	0.92	97	56	FIT OF
	5	0.92	95	55	MEAN: 0.8625
	6	0.92	96	56	
15	7	0.92	102	59	
	8	0.96	99	53	WEIBULL
	9	0.96	103	55	MEDIAN: 32.33
	10	0.96	103	55	
	11	0.96	103	55	FIT OF
	12	0.94	95	53	MEDIAN: 0.8548
20	13	0.94	103	57	
	14	0.94	100	56	
	15	0.94	100	56	MEAN
	16	0.96	104	55	M.O.R.: 55.58
	17	0.96	101	54	
	18	0.96	105	56	STD.
25	19	0.96	103	55	DEV.: 1.84
	20	0.96	100	53	
	21	0.96	107	57	

TABLE 2

Fired Slides PU

Indented Slides. These slides were fired at 400°C

and then coated with PU. No SiC whiskers were added.

5	SAMPLE			SAMPLES	
	NUMBER	DEPTH	LOAD	MOR (MPA)	22
	1	0.93	135	77	WEIBULL
	2	0.93	126	72	MEAN: 20.06
	3	0.93	127	72	
10	4	0.93	124	70	FIT OF
	5	0.92	124	72	MEAN: 0.9658
	6	0.92	132	77	
	7	0.93	128	73	
	8	0.93	133	76	WEIBULL
15	9	0.93	117	66	MEDIAN: 21.40
	10	0.93	127	72	
	11	0.9	104	63	FIT OF
	12	0.9	108	65	MEDIAN: 0.9596
	13	0.91	112	66	
20	14	0.91	114	68	
	15	0.92	116	67	MEAN
	16	0.92	120	70	M.O.R.: 70.22
	17	0.91	120	71	
	18	0.91	108	64	STD.
25	19	0.93	128	73	DEV.: 3.68
	20	0.93	125	71	
	21	0.93	121	69	
	22	0.93	127	72	

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TABLE 3

Fired slides & 6.2% SiC/PU

Indented slides & (US disp.)

These slides were fired at 400°C and then

5 coated with 6.2% SiC/PU. The coating was
dispersed with ultra sound.

SAMPLE				SAMPLES	
	NUMBER	DEPTH	LOAD	MOR (MPA)	22
10	1	0.92	240	139	WEIBULL
	2	0.92	227	132	MEAN: 4.85
	3	0.91	144	85	
	4	0.91	257	152	FIT OF
	5	0.88	128	81	MEAN: 0.8927
	6	0.88	222	141	
15	7	0.92	226	131	
	8	0.92	150	87	WEIBULL
	9	0.92	230	133	MEDIAN: 5.14
	10	0.92	162	94	
	11	0.91	243	144	FIT OF
	12	0.91	144	85	MEDIAN: 0.8758
20	13	0.87	203	132	
	14	0.87	141	91	
	15	0.88	237	150	MEAN
	16	0.88	135	86	M.O.R.: 113.47
	17	0.92	174	101	
	18	0.92	187	108	STD,
25	19	0.89	170	105	DEV.: 23.68
	20	0.89	153	95	
	21	0.92	208	121	
	22	0.92	175	102	

TABLE 4

Fired Slides & 7.6% SiC/PU

Indented Slides. These slides were fired at 400°C

and then coated with 7.6% SiC/PU. The coating was not

dispersed with ultra sound.

SAMPLE				SAMPLES	
	NUMBER	DEPTH	LOAD	MOR (MPA)	22
	1	0.92	135	78	WEIBULL
	2	0.92	137	79	MEAN: 7.57
10	3	0.93	160	91	
	4	0.93	194	110	FIT OF
	5	0.92	157	91	MEAN: 0.8326
	6	0.92	133	77	
	7	0.96	157	84	
15	8	0.96	165	88	WEIBULL
	9	0.93	145	82	MEDIAN: 8.05
	10	0.93	150	85	
	11	0.93	195	111	FIT OF
	12	0.93	126	72	MEDIAN: 0.8204
20	13	0.92	130	75	
	14	0.92	140	81	
	15	0.95	152	83	MEAN
	16	0.95	170	92	M.O.R.: 88.33
	17	0.92	157	91	
25	18	0.92	192	111	STD.
	19	0.96	143	76	DEV.: 11.95
	20	0.96	155	83	
	21	0.93	161	91	
	22	0.93	195	111	

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TABLE 5

Fired Slides & 8.8% SiC/PU

Indented slides (US disp.)

These slides were fired at 400°C and then
 5. coated with 8.8% SiC/PU. The coating was
 dispersed with ultra sound.

SAMPLE				SAMPLES
	NUMBER	DEPTH	LOAD	MOR (MPA)
10	1	0.88	171	108 WEIBULL
	2	0.88	200	127 MEAN: 6.31
	3	0.87	257	167
	4	0.87	195	126 FIT OF
	5	0.92	164	95 MEAN: 0.8461
	6	0.92	264	153
15	7	0.92	190	110
	8	0.92	250	145 WEIBULL
	9	0.93	176	100 MEDIAN: 6.71
	10	0.93	163	93
	11	0.9	180	109 FIT OF
	12	0.9	200	121 MEDIAN: 0.8348
20	13	0.93	190	108
	14	0.93	205	116
	15	0.87	180	117 MEAN
	16	0.87	177	115 M.O.R.: 114.75
	17	0.9	175	106
	18	0.9	193	117 STD.
25	19	0.93	160	91 DEV.: 19.17
	20	0.93	161	91
	21	0.91	172	102
	22	0.91	180	107

TABLE 6

Acid Washed Slides Indented

These slides were fired at 400°C then washed in
1M HNO₃. No further treatment was performed.

5	SAMPLE				SAMPLES
	NUMBER	DEPTH	LOAD	MOR (MPA)	22
10	1	0.9	110	67	WIEBULL
	2	0.9	113	68	MEAN: 16.83
	3	0.91	115	68	
	4	0.91	113	67	FIT OF
	5	0.93	115	65	MEAN: 0.9764
	6	0.93	113	64	
	7	0.91	113	67	
	8	0.91	107	63	WEIBULL
15	9	0.93	105	60	MEDIAN: 17.94
	10	0.93	105	60	
	11	0.93	100	57	FIT OF
	12	0.93	113	64	MEDIAN: 0.9691
20	13	0.93	102	58	
	14	0.93	107	61	
	15	0.9	103	62	MEAN
	16	0.9	111	67	M.O.R.: 62.96
	17	0.93	109	62	
25	18	0.93	97	55	STD.
	19	0.93	110	62	DEV.: 3.92
	20	0.93	110	62	
	21	0.94	103	57	
	22	0.94	121	67	

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TABLE 7

Acid Washed Slides & PU/SiC Indented

These slides were fired at 400°C then washed in

1M HNO₃. Then coated with PU containing 6.2% SiC whiskers

5 (US disp.)

	SAMPLE		SAMPLES		
	NUMBER	DEPTH	LOAD	MOR (MPA)	22
10	1	0.91	169	100	WEIBULL
	2	0.91	130	77	MEAN: 7.63
	3	0.87	137	89	
	4	0.87	177	115	FIT OF
	5	0.87	167	108	MEAN: 0.9498
15	6	0.87	165	107	
	7	0.93	127	72	
	8	0.93	127	72	WEIBULL
	9	0.85	160	109	MEDIAN: 8.11
	10	0.85	110	75	
20	11	0.89	161	100	FIT OF
	12	0.89	148	92	MEDIAN: 0.9370
	13	0.92	147	85	
	14	0.92	147	85	
	15	0.88	147	93	MEAN
25	16	0.88	137	87	M.O.R.: 91.10
	17	0.87	137	89	
	18	0.87	113	73	STD.
	19	0.93	165	94	DEV.: 12.40
	20	0.93	169	96	
	21	0.91	172	102	
	22	0.91	142	84	

As the fracture behaviour of the PU/SiC composite material was markedly different to the previous tests several fractures were recorded at a higher chart speed. The results of these experiments are shown in Figures 11 to 13.

The coating of glass with a composite of polyurethane and silicon carbide whiskers provides a remarkable increase in toughness. The fractured samples show a large increase in minor cracking and this provides stress dispersion (see Figures 14 and 15). When examined by scanning electron microscopy, the unfilled PU film showed a clean brittle fracture (Figure 17a), whereas the filled PU coating (Figures 17b, c) showed evidence of crack branching or tearing, while the classical scheme of fibre pull-out was demonstrated. The result of this dispersion and fibre pull-out is a large increase in the energy required to fracture the glass. The Figures 11 to 13 clearly show a very large increase in area under the stress/displacement curve for the PU/SiC composite samples (Figure 13) compared to unreinforced PU (Figure 12) or uncoated glass (Figure 11). For Figure 13 it is important to note that the curved decay in stress starting at about 1.2 mm displacement is a result of the stress being removed; it is not the ultimate failure of the sample. The stress had to be removed since the sample had curved so much as to wedge in the biaxial testing rig and further results would have had little meaning.

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Finally, it is to be understood that various other modifications and/or alterations may be made without departing from the spirit of the present invention as outlined herein.

CLAIMS :

1. A glass coating composition including
an effective amount of at least one inorganic or
organic polymeric component; and

5 at least one reinforcing component incorporated
therein;

the glass coating composition being such that when
coated on a glass substrate it strengthens and toughens the
article.

10 2. A glass coating composition according to claim 1
wherein the at least inorganic or organic polymer component
is a synthetic organic polymer selected from acrylate and
methacrylate polymers or copolymers, acrylamide or
methacrylamide polymers or copolymers, urethane polymers or
copolymers, alkyd resins or mixtures thereof.

15 3. A glass coating composition according to claim 2
wherein the synthetic organic polymers includes
approximatley 40% to 90% by weight, based on the total
weight of the glass coating composition, of a polyurethane
polymer.

20 4. A glass coating composition according to claim 1
wherein the at least one reinforcing component is selected
from components which have a platelet-type structure or a
fibrous structure.

25 5. A glass coating composition according to claim 4
wherein the reinforcing component is selected from silicon
carbide or vermiculite having a platelet type structure and
silicon carbide, silicon nitride, alumina and metals having
a fibrous structure; or mixtures thereof.

6. A glass coating composition according to claim 5

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wherein the at least one reinforcing component includes approximately 5 to 60% by weight, based on the total weight of the glass coating composition, of an exfoliated vermiculite.

5. 7. A glass coating composition according to claim 1 further including an effective amount of at least one coupling agent.

10. 8. A glass coating composition according to claim 7 wherein the at least one coupling agent includes approximately 0.1 to 1% by weight, based on the total weight of the glass coating composition, of an amino silane.

15. 9. A glass coating composition according to claim 2 wherein, when the synthetic organic polymer is a water-soluble polymer, the glass coating composition further includes an effective amount of at least one cross-linking agent.

20. 10. A glass coating composition according to claim 9 wherein the at least one cross-linking agent is present in amounts of from 0.1% to approximately 50% by weight, based on the total weight of the glass coating composition, of a heat or radiation curable cross-linking agent.

11. 11. A glass coating composition according to claim 1 including

25. approximately 40 to 70% by weight of polyacrylamide; approximately 30 to 60% by weight of vermiculite; and approximately 0.1% to approximately 0.5% by weight of (N,N-diethyl-3-aminopropyl)trimethoxysilane.

12. 12. A glass coating composition according to claim 1 including

approximately 80 to 95% by weight of a polyurethane polymer; and

approximately 5 to 15% by weight of silicon carbide.

13. A toughened article including

5 a glass article; and

a glass coating on at least one surface thereof formed from a glass coating composition including an effective amount

10 at least one inorganic or organic polymeric component;

and

at least one reinforcing component incorporated therein;

the glass coating being such that when coated on the glass article, it strengthens and toughens the article.

15 14. A toughened article according to claim 13 wherein the glass article is formed from a silica based glass.

16. A toughened article according to claim 13 wherein the glass coating composition includes

approximately 40 to 70% by weight of polyacrylamide;

20 approximately 30 to 60% by weight of vermiculite; and

approximately 0.1% to approximately 0.5% by weight of a coupling agent.

25 16. A toughened article according to claim 15 wherein the coupling agent is (n,n-diethyl-3-aminopropyl)-trimethoxy-silane.

17. A toughened article according to claim 13 wherein the glass coating composition includes

approximately 80 to 95% by weight of a polyurethane polymer; and

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approximately 5 to 15% by weight of silicon carbide.

18. A toughened article according to claim 13 wherein the glass article is subjected to a purification step prior to application of the coating.

5. 19. A process for preparing a toughened article including providing a glass article; and a glass coating composition including an effective amount of at least one inorganic or organic polymeric component; and 10 at least one reinforcing component incorporated therein; the glass coating composition being such that when coated on a glass substrate it strengthens and toughens the article; 15 contacting the surface of the glass article with the glass coating composition; and drying the coated glass article so formed.

20. A process according to claim 19 further including providing at least one coupling agent; and mixing the coupling agent with the polymeric component and at least one reinforcing component for a time sufficient to allow the coupling component to hydrolyse and/or to interact with the reinforcing component prior to contact of the surface of the glass article.

25. A process for preparing a toughened article according to claim 19 wherein the at least one reinforcing agent is a vermiculite, said process further including the preliminary step of

subjecting the vermiculite to a conversion proces to

produce an exfoliated vermiculite.

22. A process for preparing a toughened article according to claim 18 which process further includes the preliminary step of subjecting the glass article to a heat treatment elevated temperature for a time sufficient to clean the surface thereof.

23. A process for preparing a toughened article according to claim 21 wherein the heat treatment is conducted at temperatures approximately 350-450°C.

10 24. A process for preparing a toughened article according to claim 18 wherein the polymeric component is a water soluble organic polymer which process further includes providing an effective amount of at least one cross-linking agent; and

15 subsequently curing the coated glass article.

25. A process for preparing a toughened article according to claim 23 wherein the at least one cross-linking agent is a heat curable cross-linking agent and the curing step includes heating the coated glass article at elevated temperature for a period sufficient to provide substantially complete cure.

20 26. A process for preparing a toughened article substantially as hereinbefore described with reference to any one of the examples.

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Fig. 1.

UNCOATED GLASS

STRESS VERSUS DISPLACEMENT

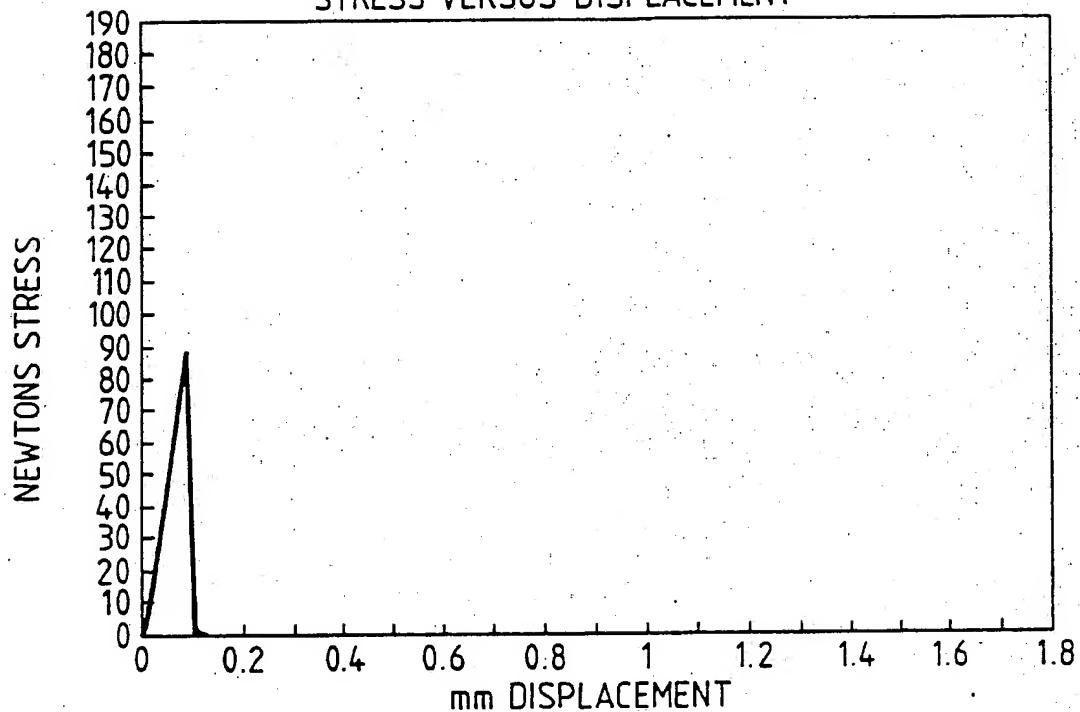
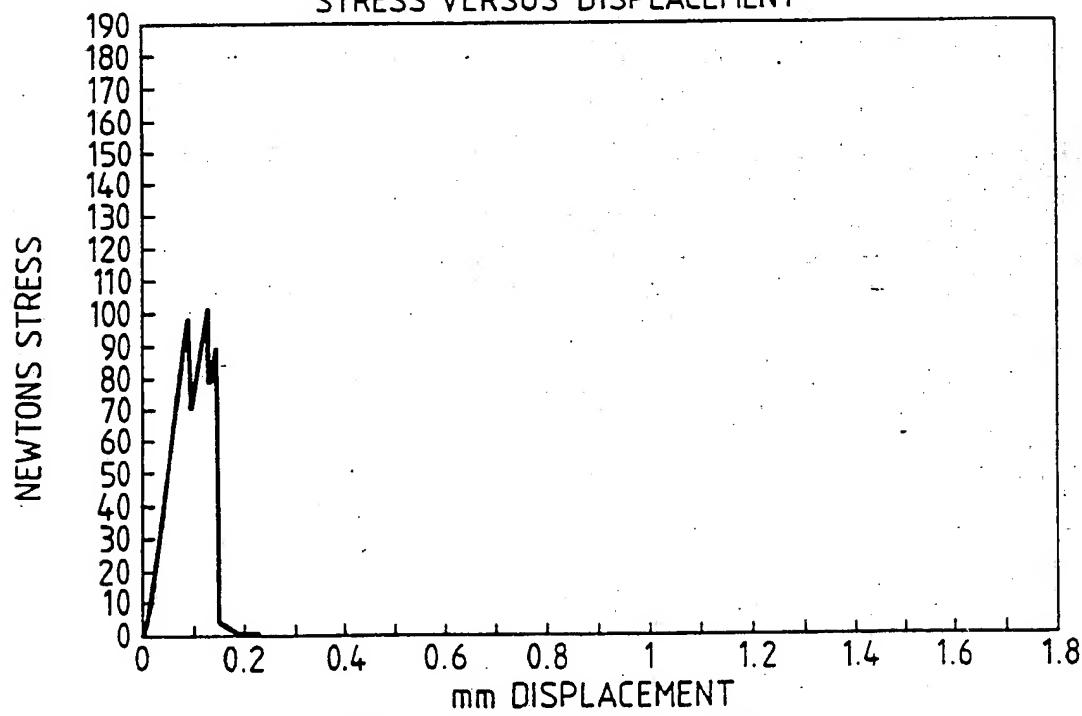


Fig. 2.

PU COATING - NO WHISKERS

STRESS VERSUS DISPLACEMENT



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Fig.3. PU/SiC COMPOSITE ON GLASS
STRESS VERSUS DISPLACEMENT

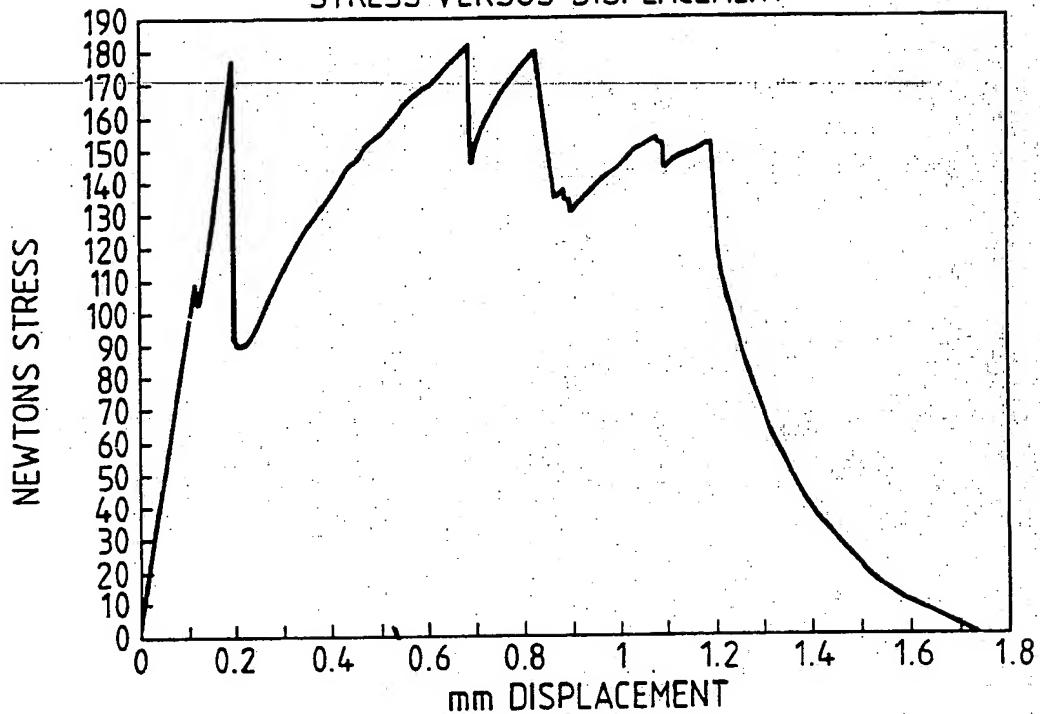
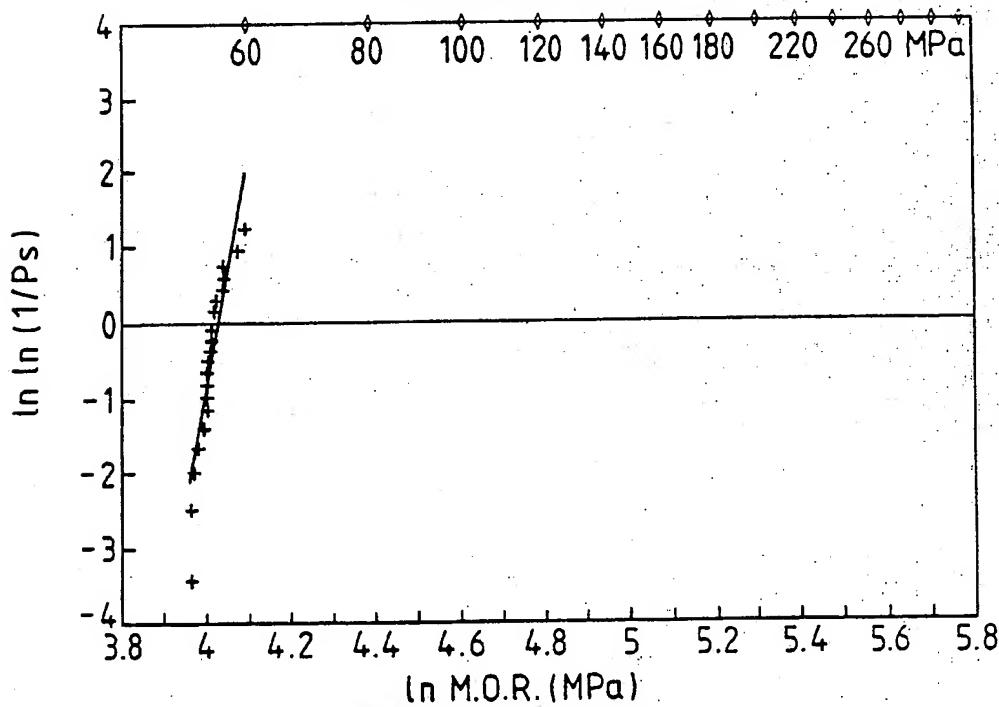


Fig.4. AS FIRED SLIDES, UNCOATED
INDENTED / REFIRED



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Fig.5. FIRED SLIDES PU
INDENTED SLIDES

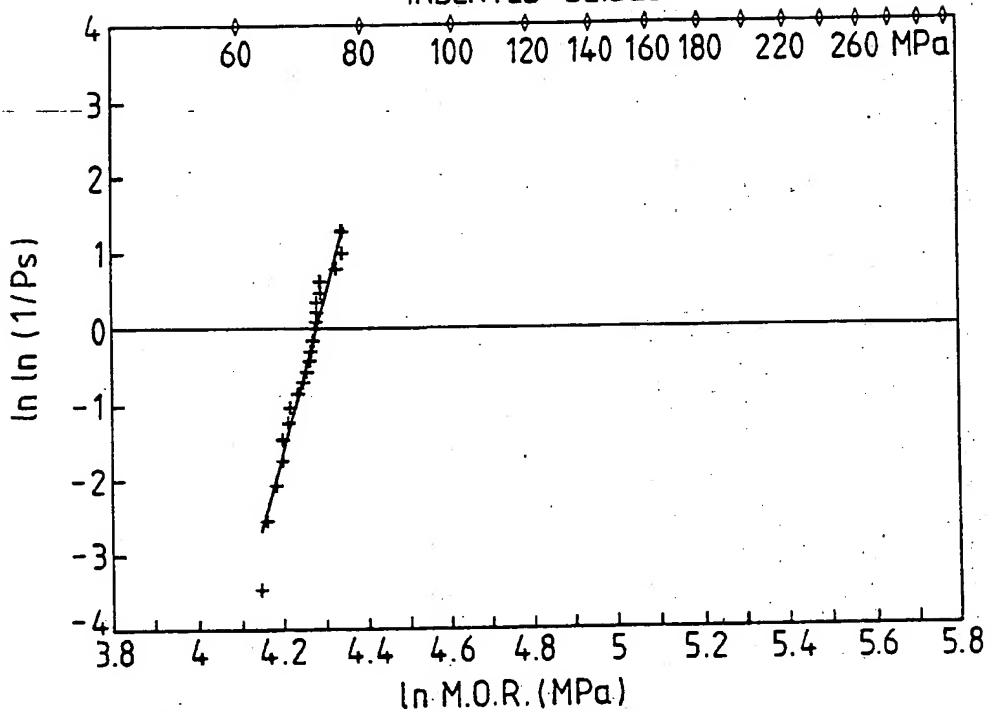
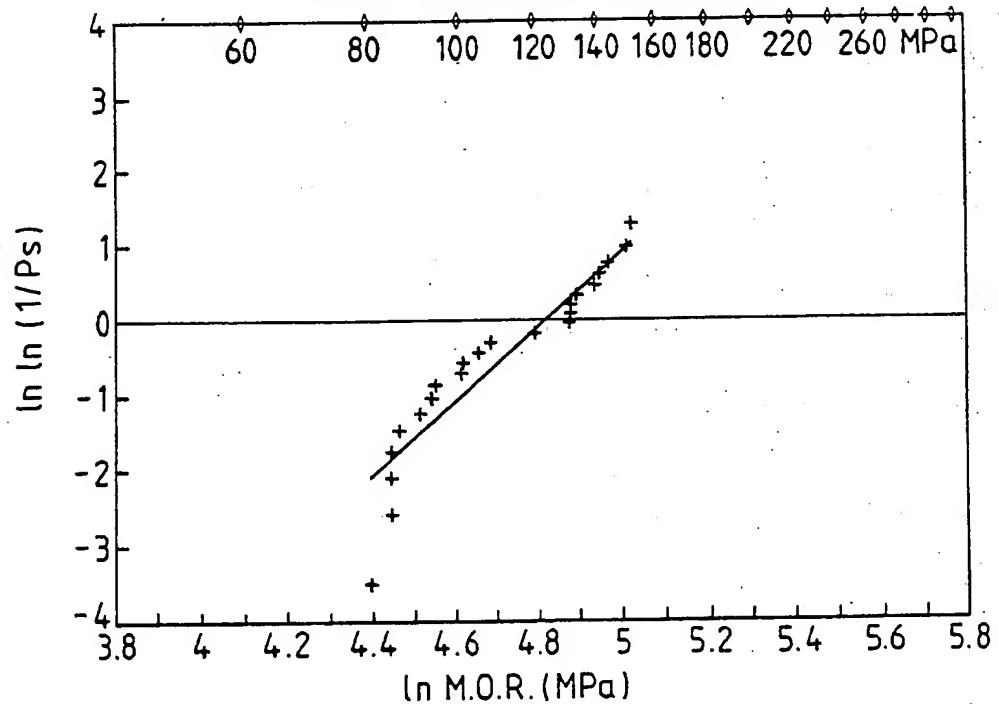


Fig.6. FIRED SLIDES & 6.2% SiC/PU
INDENTED SLIDES (US DISP.)



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Fig. 7. FIRED SLIDES & 7.6% SiC/PU
INDENTED SLIDES

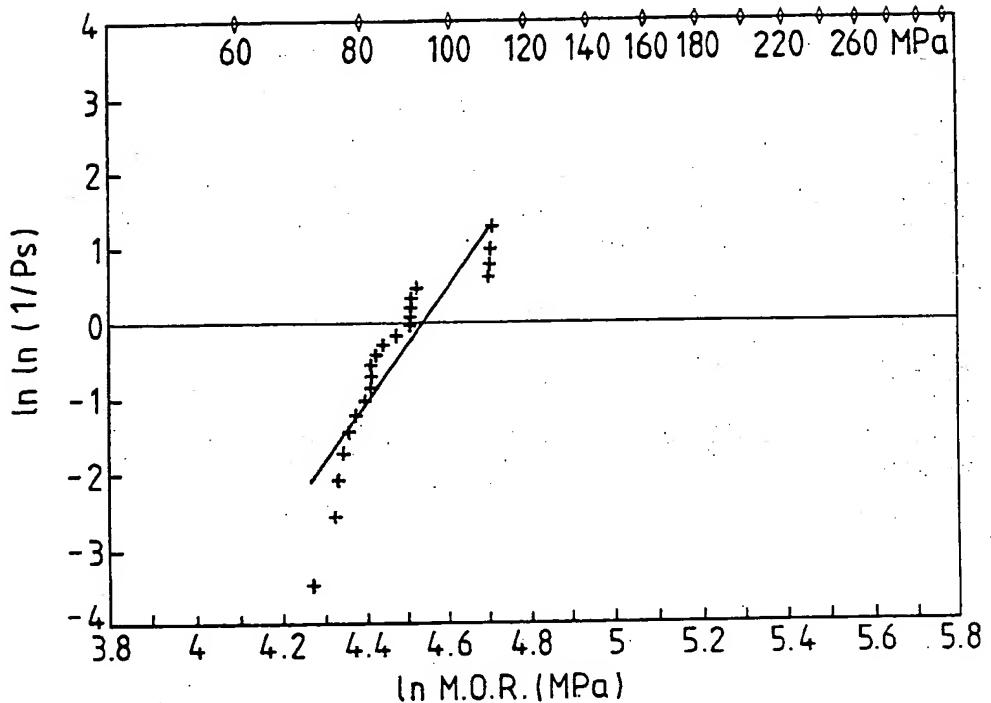
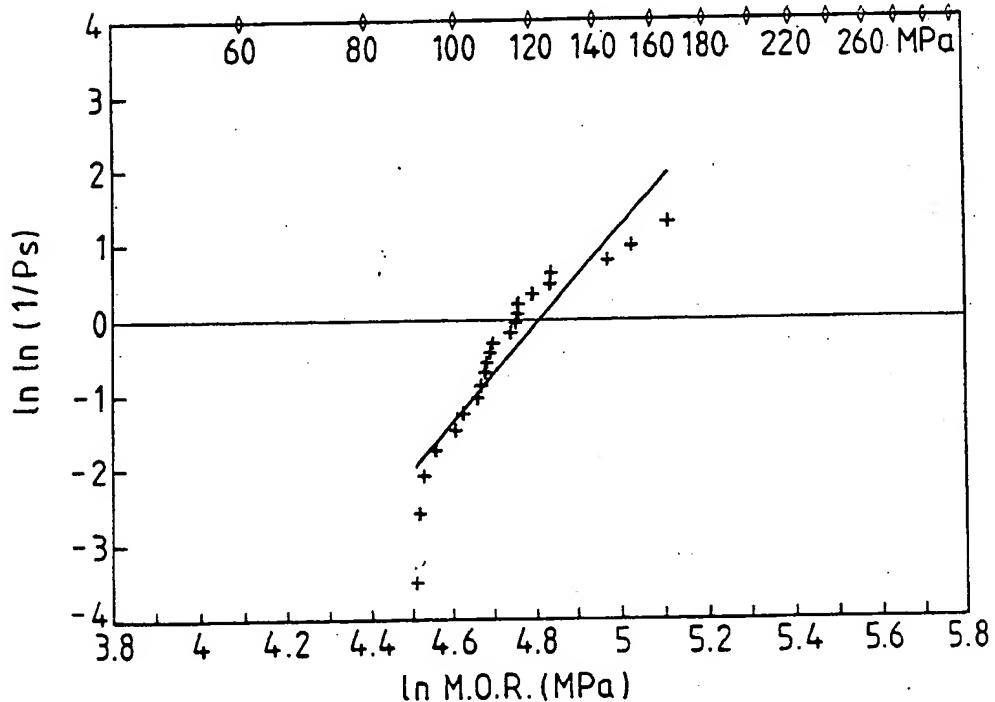


Fig. 8. FIRED SLIDES & 8.8% SiC/PU
INDENTED SLIDES (US DISP.)



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Fig. 9. ACID WASHED SLIDES
INDENTED

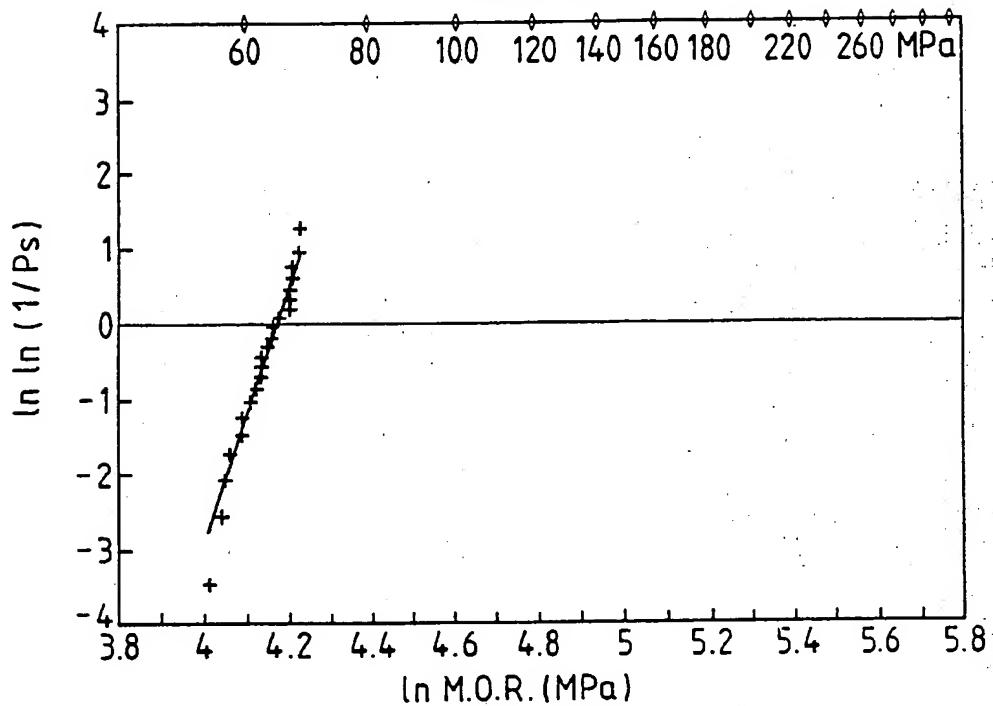
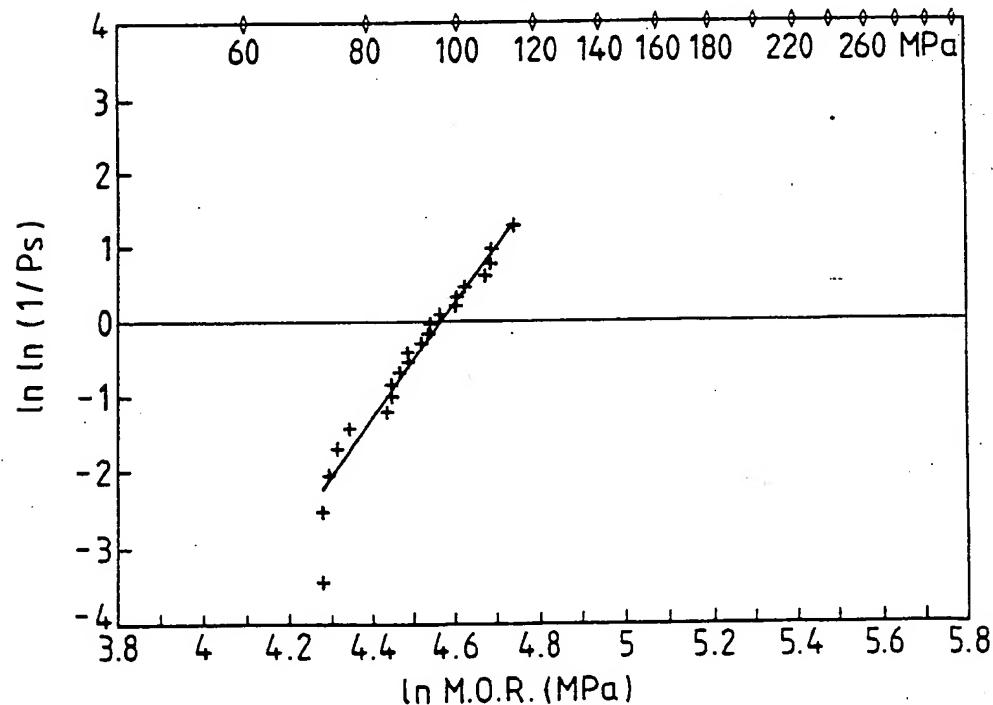


Fig. 10. ACID WASHED SLIDES & PU/SiC
INDENTED



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Fig. 11.

UNCOATED GLASS

STRESS VERSUS DISPLACEMENT

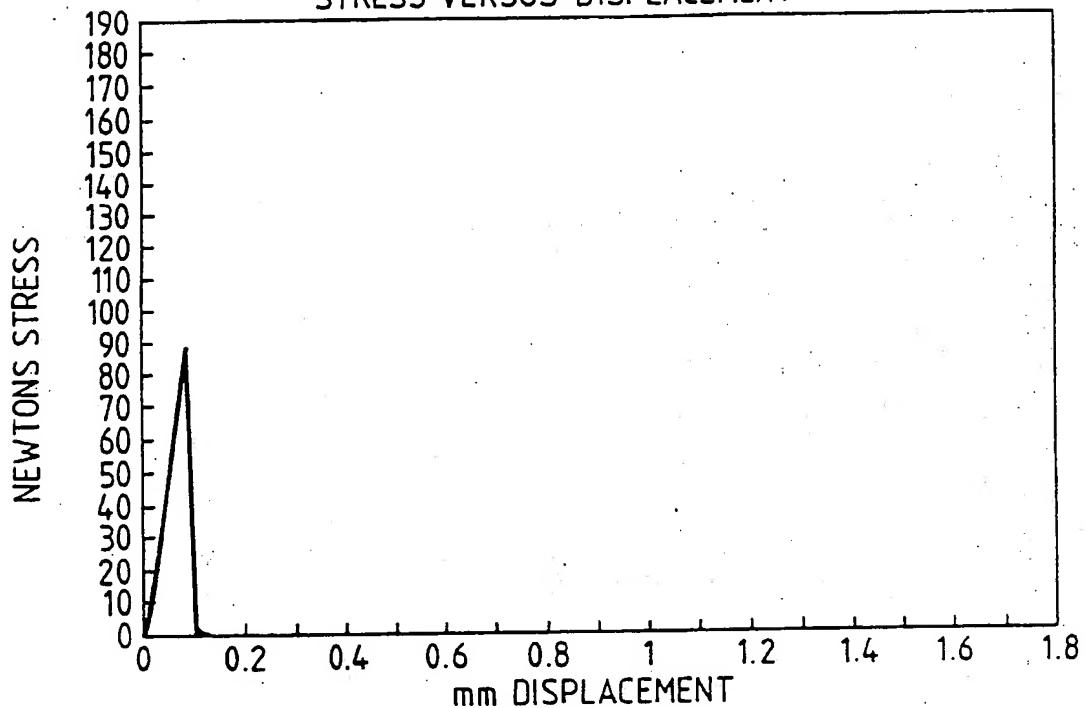
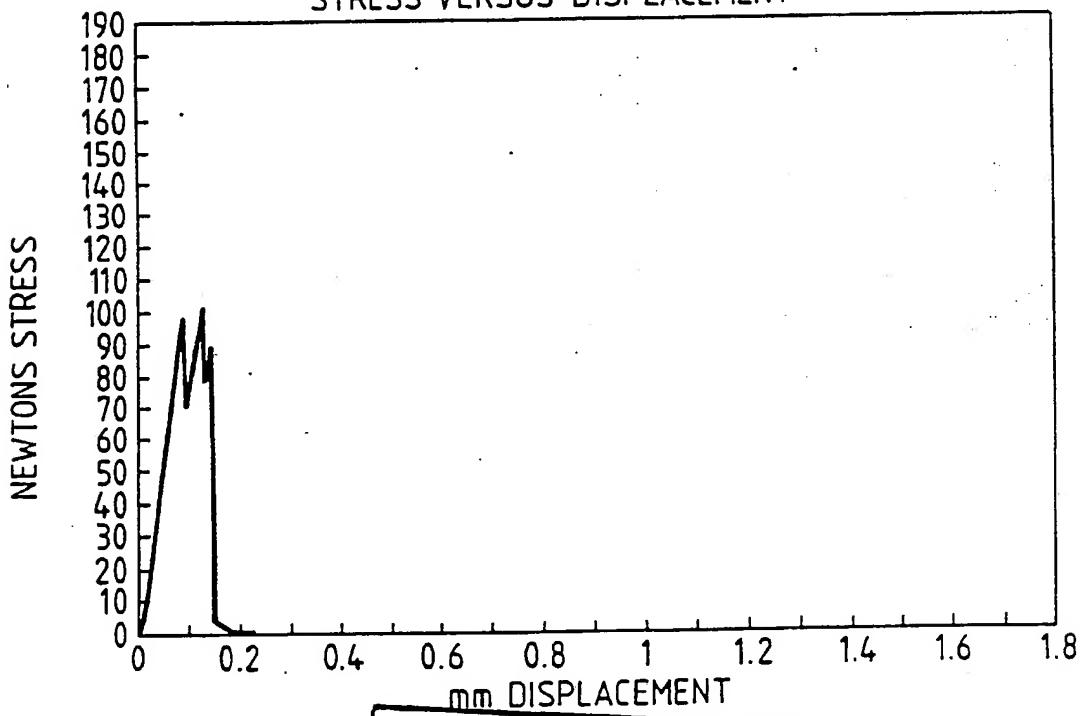


Fig. 12.

PU COATING - NO WHISKERS

STRESS VERSUS DISPLACEMENT



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Fig.13. PU/SiC COMPOSITE ON GLASS
STRESS VERSUS DISPLACEMENT

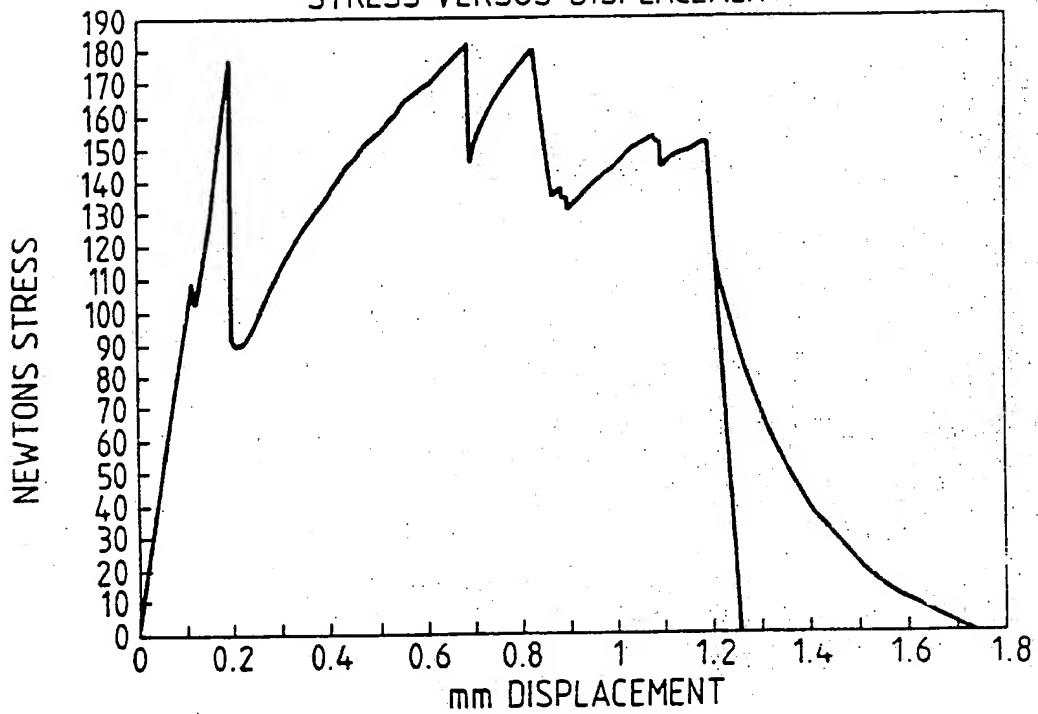
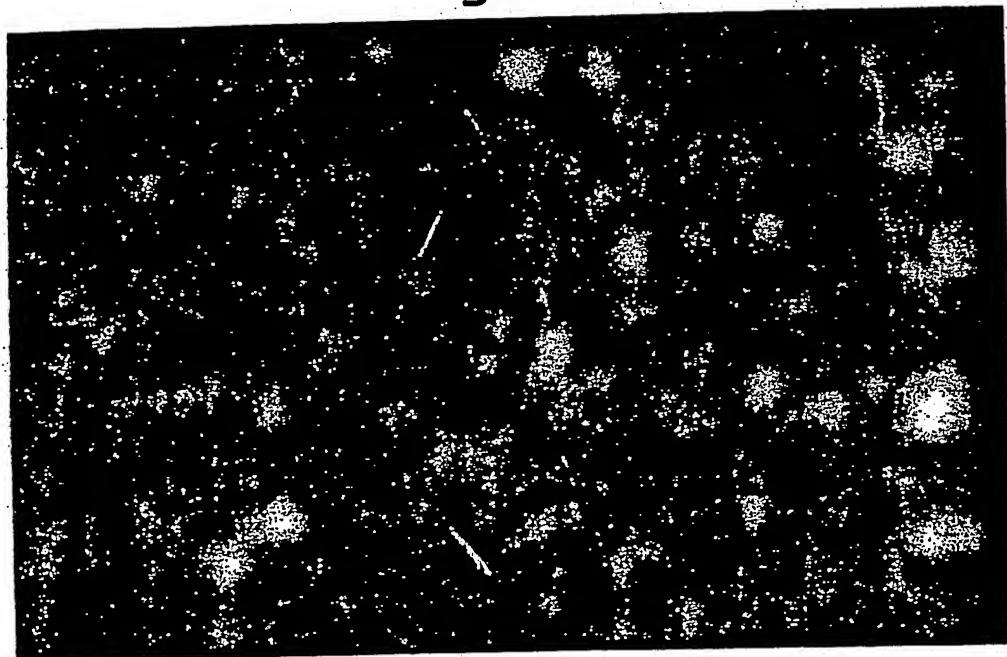


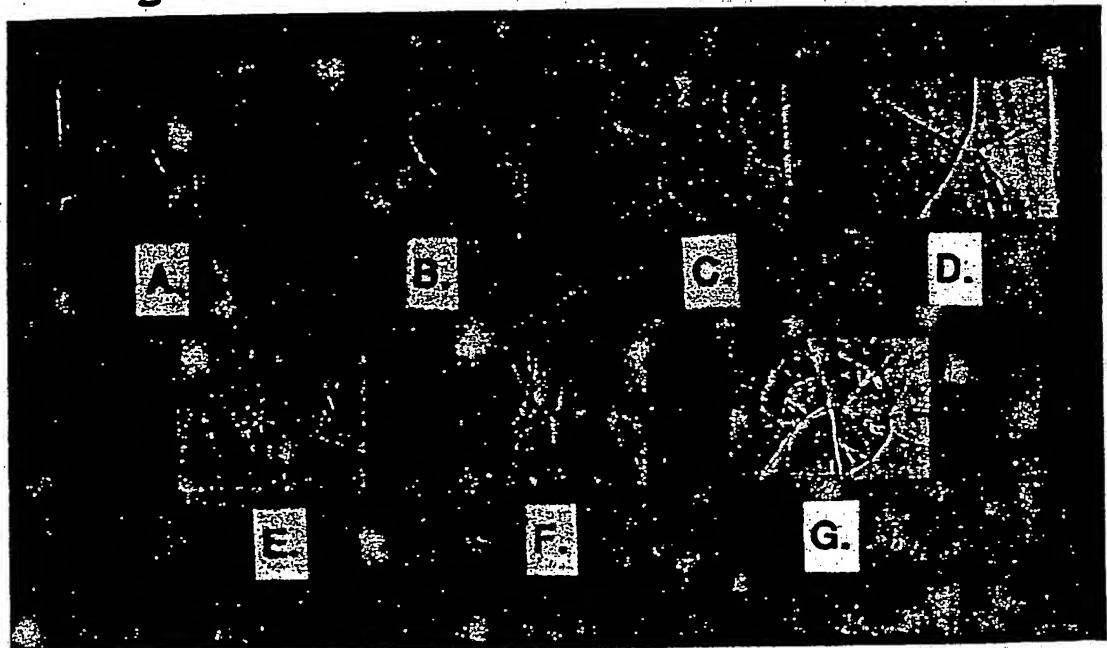
Fig.14.



THE DEVELOPMENT OF MINOR CRACKING DURING FRACTURE
OF A GLASS SLIDE COATED WITH PU/SiC COMPOSITE.

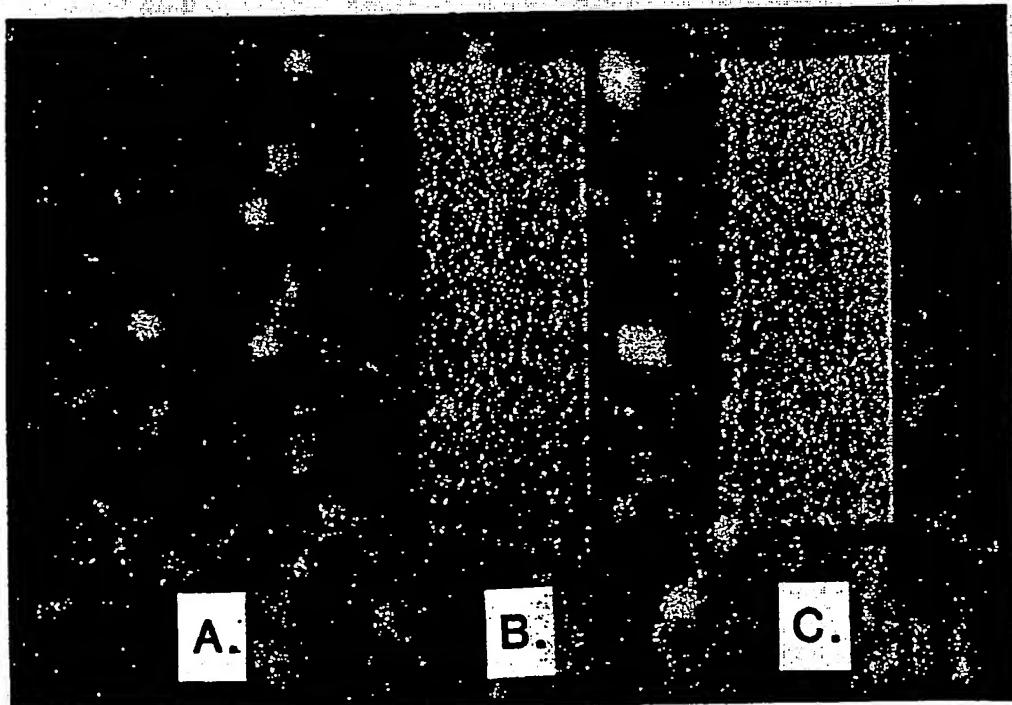
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Fig. 15.



FRACTURED GLASS SLIDES:
A & B NORMAL UNCOATED SLIDES
C - G SLIDES COATED WITH PU/SiC COMPOSITE.

Fig. 16.

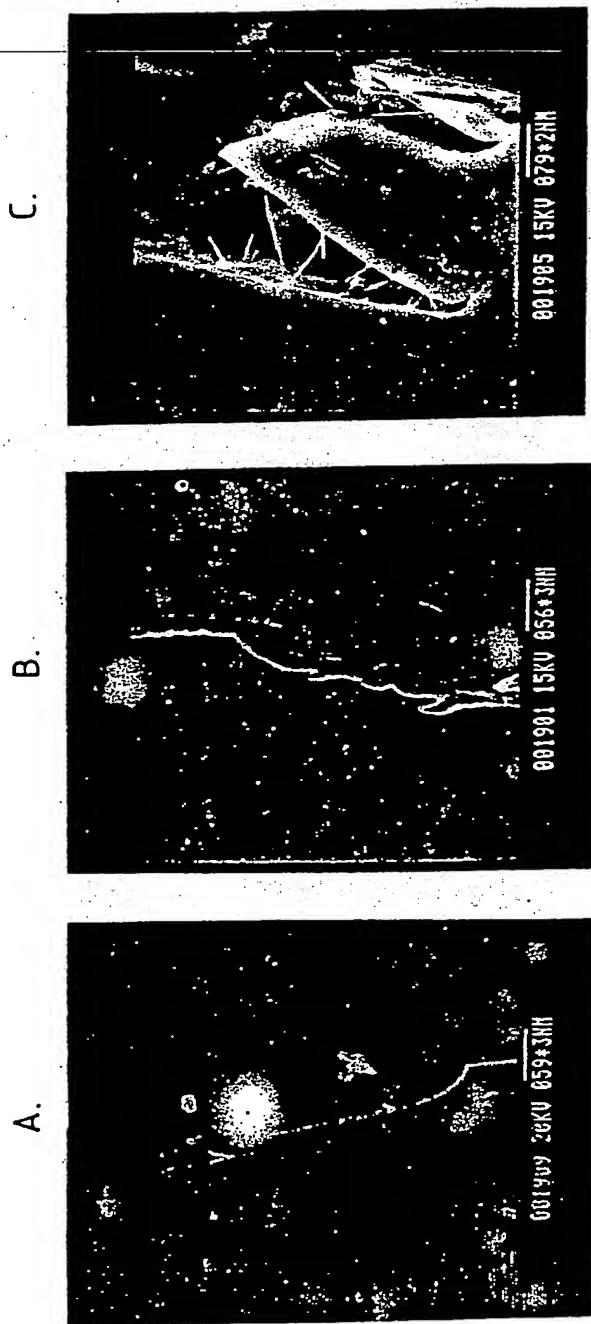


PU COATED SLIDES PRIOR TO FRACTURE :
A UNREINFORCED PU
B PU/SiC DISPERSED BY STIRRING.
C PU/SiC DISPERSED BY ULTRA SONIC BATH.

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Fig. 17.



SEM PHOTOGRAPHS OF CRACKS IN PU/SiC FILMS.

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INTERNATIONAL SEARCH REP'T

International Application No. PCT/AU 89/00196

I. CLASSIFICATION OF SUBJECT MATTER (if several classification symbols apply, indicate all) 6

According to International Patent Classification (IPC) or to both National Classification and IPC

Int. Cl.⁴ C03C 17/32, B32B 17/04

II. FIELDS SEARCHED

Minimum Documentation Searched 7

Classification System	Classification Symbols
IPC	C03C 17/32, B32B 17/04

Documentation Searched other than Minimum Documentation
to the Extent that such Documents are Included in the Fields Searched 8

AU : IPC as above

III. DOCUMENTS CONSIDERED TO BE RELEVANT 9

Category*	Citation of Document, ¹¹ with indication, where appropriate, of the relevant passages 12	Relevant to Claim No 13
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A	AU,B,58802/80 (525770) (SEKISUI KAGAKU KOGYO KK and TOKUYAMA SEKISUI KOGYO KK) 4 December 1980 (04.12.80)	
A	AU,B,41860/85 (583038) (SAINT-COBAIN VITRAGE) 7 November 1985 (07.11.85)	
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A-	US,A,3805985 (HAGIWARA ET AL) 23 April 1974 (23.04.74)	
A	US,A,4143181 (CAHN ET AL) 6 March 1979 (06.03.79)	
A	US,A,4280944 (SAITO ET AL) 28 July 1981 (28.07.81)	
A	US,A,4510282 (GOLL) 9 April 1985 (09.04.85)	

* Special categories of cited documents: 10 "T" later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention

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"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)

"O" document referring to an oral disclosure, use, exhibition or other means

"P" document published prior to the international filing date but later than the priority date claimed

"X" document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step

"Y" document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art.

"&" document member of the same patent family

IV. CERTIFICATION

Date of the Actual Completion of the
International Search
14 July 1989 (14.07.89)

Date of Mailing of this International

Search Report

121 July 1989 (21.07.89)

International Searching Authority

Signature of Authorized Officer

Australian Patent Office

P. Malano
P. MALANO ASE

ANNEX TO THE INTERNATIONAL SEARCH REPORT ON
INTERNATIONAL APPLICATION NO. PCT/AU 89/00196

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

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					US 4389508
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		FR	2563754	IN	164462
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